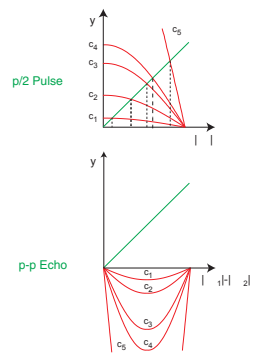


Towards Using Radiation Damping to Improve Sensitivity

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Field Inhomogeneity

Transcendental Solution



Radiation damping dynamics in both narrow line and homogeneously broadened systems are well understood. Introduction of magnetic field inhomogeneity necessarily complicates the radiation damping problem, and consequently, a complete analytical description has not yet been demonstrated. Initial work in this area led to a relationship between the initial tipping angle α_0 of the on resonance central vector of a symmetric field distribution $M(0)$ and the change in tipping angle $[D]$ due to the combined torque of radiation damping and the inhomogeneous magnetic field. The resulting area theorem generated from the Bloch equations using a transformation first realized in the treatment of self-induced transparency in optical systems can be written in terms of the radiation damping rate $1/T_R = 2M_0Q\mu_0$ and the inverse linewidth for a Lorentzian distribution $1/T_2^*$ as

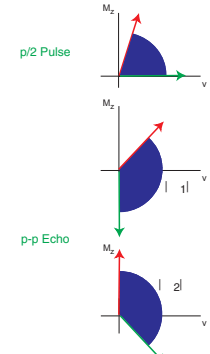
$$[D] = (T_2^*/T_R)\sin(\alpha_0 - [D])$$

This angle change $[D]$ also represents the area of the measured time domain signal following a α_0 pulse. Graphical solutions to this transcendental equation for $\alpha_0 = p/2$ and several choices of $c_n = T_2^*/T_R$ are shown on the top left. The diagram shown on the top right describes the net effect of the rotation of $M(0)$ from the z direction at $t=0$ to the M_z direction at a time later when all of the effects of radiation damping have vanished. Extension of this analytical approach to two and many μ pulses yields a series of transcendental relations such as that shown above. In the special case of two μ pulses separated by a time long enough for radiation damping to vanish, one recovers the relation

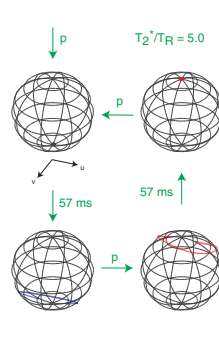
$$[D_2] \cdot [D_1] = (T_2^*/T_R)\sin(\alpha_0 - [D_2])$$

Graphical solutions to this equation are shown on the lower left for various choices of c_n . Since intersection of the linear curve representing $y = [D_2] \cdot [D_1]$ with any of the curves $y = (T_2^*/T_R)\sin(\alpha_0 - [D_2])$ only occurs at the origin, $[D_2] = [D_1]$. The consequences of this equality are shown beginning with the middle diagram on the right. Following a μ pulse $M(0)$ at $t=0$ is aligned along the $-M_z$ direction as shown by the green arrow. The combined effect of radiation damping and field inhomogeneity rotate $M(0)$ toward the $-M_x$ direction by an angle $[D_1]$ as shown by the red arrow. Application of a second μ pulse transforms the red arrow into the green arrow shown in the diagram on the lower right. Again radiation damping and the inhomogeneous field rotate this vector to the $-M_z$ direction due to the equality $[D_2] = [D_1]$. Although only appropriate for $M(0)$, this theorem serves as a guide to the development of a three component echo. Indeed both

Vector Model



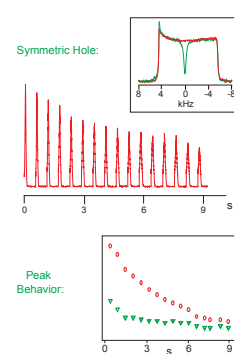
Sphere Hopping



SEDOR Analogue

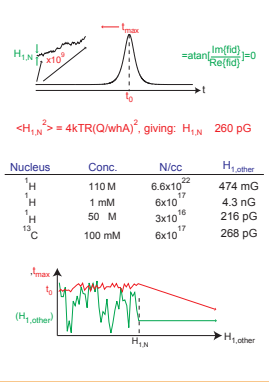
Although the analytical theorem is only appropriate for describing total rotation angles $[D_2]$ for $M(0)$ from $t=0$ until times when the reaction field due to all of the isochromats is averaged to zero, the idea of three component refocusing predicted by this theorem can be used as an indirect detector. The diagram on the left is appropriate for a symmetric Lorentzian distribution having $T_2^*/T_R = 5.0$. An initial μ pulse inverts all of the isochromat vectors, designated by a blue spot at the south pole of the sphere shown on the top left. After 57 ms, the vectors have fanned out in three dimensions shown on the bottom left sphere. For this particular choice of T_2^*/T_R , 57 ms corresponds to the maximum integrated transverse magnetization or signal. Application of a second μ pulse transforms this distribution into the sphere shown on the bottom right. As time proceeds

Hole Burning

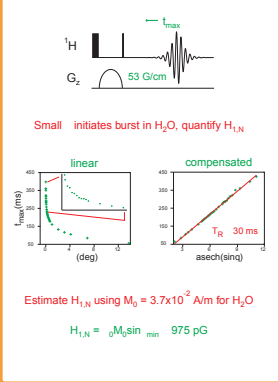


Trigger Detector

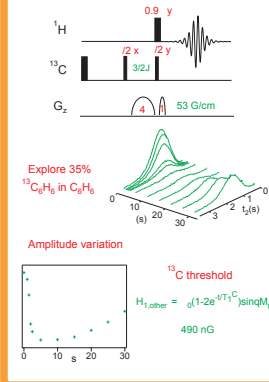
Burst Modulation



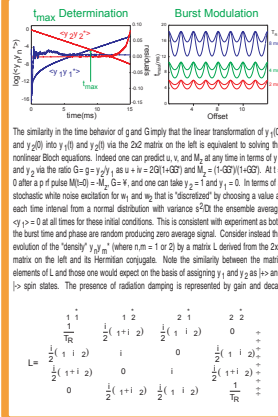
DRX 500 Nonideality



Threshold Considerations



Startup Considerations



Again thermal noise in the circuit causes incoherent fluctuations in the xy field experienced by the magnetization. Modeling these changes in w_1 and w_2 with the same "stochastic" white noise mentioned above now provides non-zero values for $\langle y_1 y_1 \rangle$ and $\langle y_2 y_2 \rangle$. In terms of the time step weighted variance $\langle y^2 \rangle$, the time evolution of these components is given by:

$$\frac{d}{dt} \langle \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \cdot \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \rangle = \frac{1}{T_R} \langle \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \cdot \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \rangle + \langle \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \cdot \begin{pmatrix} y_1 \\ y_2 \end{pmatrix} \rangle$$

The numerical average of $\langle y_1 y_1 \rangle$ and $\langle y_2 y_2 \rangle$ over 1000 particles is shown graphically as tick lines in the top left graph for $T_R = 2 \text{ ms}$, $s^2 = 0.5 \text{ rad}^2/\text{ms}$, and $De = 0.5 \text{ rad/ms}$. An analytical solution based on the above matrix equation yields curves essentially identical to those shown on the figure. The residuals between numerical computation of $\langle y_1 y_1 \rangle$ and $\langle y_2 y_2 \rangle$ and the approximation are also included in the diagram to demonstrate the accuracy of the analytical model. Comparison of the intersection point of these two curves with single particle values for y_1 indicates that this particular time describes the average burst time t_{max} . Equating the analytical solutions deduced from the above matrix equation yields the startup time

$$t_{max} = \frac{1}{\frac{1}{T_R} - \frac{1}{2}} \ln \left(\frac{1 + \frac{1}{2T_R}}{1 - \frac{1}{2T_R}} \right)$$

It is interesting to ask how much coherent xy field is necessary to dominate and shorten t_{max} to determine whether or not a trigger based detection strategy is possible. Proceeding in exactly the same way as above in the determination of $\langle y_1 y_1 \rangle$ and $\langle y_2 y_2 \rangle$ leads to the relation

$$\frac{1}{T_R} = \frac{1}{2} \left(\frac{1 + \frac{1}{2T_R}}{1 - \frac{1}{2T_R}} \right)$$